# **USERS MANUAL FOR** GODDARD ORBIT DETERMINATION PROGRAM

**April 1965** 

Contract No.: NAS-5-3509

Prepared by

**Sperry Rand Systems Group Sperry Gyroscope Company Division of Sperry Rand Corporation** Great Neck, New York (Sperry Report No. AB-1210-0038-2)

for

Goddard Space Flight Center Greenbelt, Maryland

N66 87141

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#### INTRODUCTION

The information in this manual is intended as a guide to those desiring to use the Orbit Determination Program. The material herein has been divided into four main sections.

Section 1. contains a general description of program usage. It discusses the major subdivisions of the program and each of their sub-modes. Also covered in this section are the various options available to the user in each subdivision.

Section 2. is devoted to a complete description of how program input is to be set up. This section lists by name all variables which may be read in. It gives the input section number, location by card count, the format and description of each input variable.

Section 3. provides a complete description of the output available to the user. It explains how the frequency of output may be controlled. The options available in each subdivision are listed and the method by which they are specified by the user is explained.

In Section 4., a description is given of operating procedures to be followed in the running of the Orbit Determination Program. A typical deck set-up is included for the user's information and tape assignments are discussed. There is a discussion of the two sub-programs into which Subdivision B2 has been divided. Some recommended procedures for operating efficiency are also described.

This manual was prepared under Contract NAS-5-3509 for the Theoretical Division (Special Projects Branch) of the Goddard Space Flight Center, Greenbelt, Maryland.

#### 1.0 GENERAL DESCRIPTION OF PROGRAM USAGE

The program is coded entirely in the FORTRAN IV language and runs under the IBSYS/IBJOB operating system. It has three major subdivisions, viz.,

- a) A Mode Computation of vehicle ephemeris and generation of associated observations;
- b) Bl Mode Statistical processing of data considering just six basic states (three position and three velocity);
- c) B2 Mode Ctatistical processing of data with capability of specifying up to twenty additional states.

The following sections will describe these subdivisions in more detail.

#### 1.1 A MODE

This subdivision can be broken down into four sub-modes:

- a) The computation of vehicle ephemeris only;
- b) Generation of observations for up to twenty-five ground stations and one on-board system; both observations and ephemeris printed;
- c) Same as (b) with the additional facility for writing observations onto tape in a format suitable for processing by subdivisions Bl and B2;
- d) Down range prediction, in which the following are standard outputs:
  - i) the time at which a vehicle comes in view of a ground station;
  - ii) the total time in sight
  - iii) observation quantities while in sight
  - iu) the time of polar baseline and meridian crossings

#### 1.1.1 TRAJECTORY COMPUTATION OPTIONS

The user has the option of selecting either the Encke or Cowell special perturbation technique or of suppressing all perturbations and using the two-body solution alone.

The Encke integration is single precision, the two-body component being computed in double precision. The Cowell method is double precision throughout.

The perturbations available to the user include the sun, moon, and five near planets, 38 harmonic coefficients of the earth's oblateness, solar radiation pressure, air drag and thrust. The planets contributing perturbations can be individually selected as can the total number and order of each individual harmonic coefficient. The air density tables are composed of the U.S. Standard Atmosphere of 1962 (up to 250 km.) and Harris—Preister Tables from 100 km. up to 1100 km. In the overlapping regions, an average of the values given by the two models is used.

The Harris-Priester model is a function of solar flux, altitude and local sun time. Solution for the density from these tables requires interpolation in all three variables.

The solar pressure routine contains provisions for computing the solar illumination factor as continuously variable from 1 to 0 as the vehicle travels from full sunlight through penumbra into the umbral region.

The integrator used in both the Encke and Cowell methods is a modified Adams method due to Nordsieck. The step size can be varied at any time during a run on a continuously variable basis, thereby eliminating the need of switching to Runge-Kutta-Gill to attain times not integral increments of the step size. Runge-Kutta-Gill is nonetheless required as a starting procedure for the Nordsieck method.

#### 1.1.2 OTHER OPTIONS

The following observations can be generated:

- a) Azimuth
- b) Elevation
- c) Range
- d) Range-Rate
- e) Hour-Angle

- f) Declination
- g) l direction cosine
- h) m direction cosine
- i) X Antenna Angle
- j) y Antenna Angle
- k) Range equivalent
- 1) Range-rate equivalent
- m) One way Doppler
- n) Two way Coherent Doppler
- o) Two Way Pseudo Doppler
- p) Radar Altimeter Ranging
- q) Stadiometric Ranging
- r) Planet to Planet Angle
- s) Star to Planet Angle
- t) Star to Landmark Angle
- u) Landmark to Landmark Angle
- v) Radar Occultation
- w) Star Occultation

The user can input initial conditions in several coordinates and in several systems of units, at his option. In addition to these coordinate system options, the input conditions can be precessed, nutated, and librated for conversion to the proper inertial system.

The input is set up so that a run can be made using many items that are considered standard. Such items include print intervals, rectification criteria, integration intervals and similar variables. These standard inputs have three degrees of precision. That is, step size and rectification criteria, the number of planets and number of harmonics in oblateness are a function of precision and accuracy requirements. The user has a choice of three levels. If the standards are not to his liking, however, he can overwrite any or all of them by using

additional input information.

Other options include the application of precession, nutation and libration transformations to the oblateness of the earth and moon, and the printing of times when the vehicle crosses into and out of the penumbral region of the reference body. In the case of the earth-moon system, passage of the vehicle into and out of these same regions for the non-reference body is also available for printing out.

#### 1.2 B1 MODE

In this subdivision, the user has a choice of one of six sub-modes:

- a) Orbit determination, including the processing of real data;
- b) Orbit determination using artificial data with the addition of noise;
- c) Error Analysis
- d) Propagation of Covariance matrix
- e) Propagation of Miss Coefficients
- f) Data Scanning

The first three modes involve the reading of a properly formatted data tape. In the first mode real data is used while in the second the tape contains simulated errorless data, to which noise with selected random error can be applied. In the third mode, the program assumes zero observation error so that the nominal trajectory is followed and the covariance matrix reflects the error under true tracking conditions.

The fourth mode provides for propagation of the covariance matrix along a nominal trajectory when data are not available and the fifth mode provides miss coefficients.

The sixth mode reads the data tape and computes residuals between the data and the assumed trajectory. This information allows the user to find bad data points which are not usually obvious when the raw data are scanned.

#### 1.2.1 OTHER OPTIONS

The added options which the user has at his disposal include:

- a) a flexible print system;
- b) ability to reject data of any type from any station;
- c) ability to ignore data of a given type and from a given station until a specified time;
- d) ability to specify N and then have one of each Nth observation of a given type from a given station processed;
- e) application of refraction correction;
- f) selection of corrections for time delay
- g) ability to reject data whose residual exceeds a specified statistical level:
- h) provision of statistical uncertainty of each observation type as input;
- i) provision to print, in summary form, observation time, station number, observed value and residual of each point processed.

#### 1.3 B2 MODE

This subdivision allows the user to consider as states up to twenty additional variables. These twenty variables can be chosen from a total of some 800 different variables. For example, states can be chosen from all of the planetary gravitational parameters, all of the oblateness harmonics of the earth and moon, the velocity of light, solar flux and area—to—mass ratio of the satellite.

Further, for each of the twenty—five stations, three components of station location, three components of station angular orientation, six components of refraction, and a bias error in each observation type can be selected.

Other features of this maximum state version are identical to those of the minimum state version. Both a Bayes and a minimum variance version are available with both Cowell and Encke integrators. In each version, the input options discussed previously are available. The only difference is that no provisions for handling powered flight are included in the B2 subdivision.

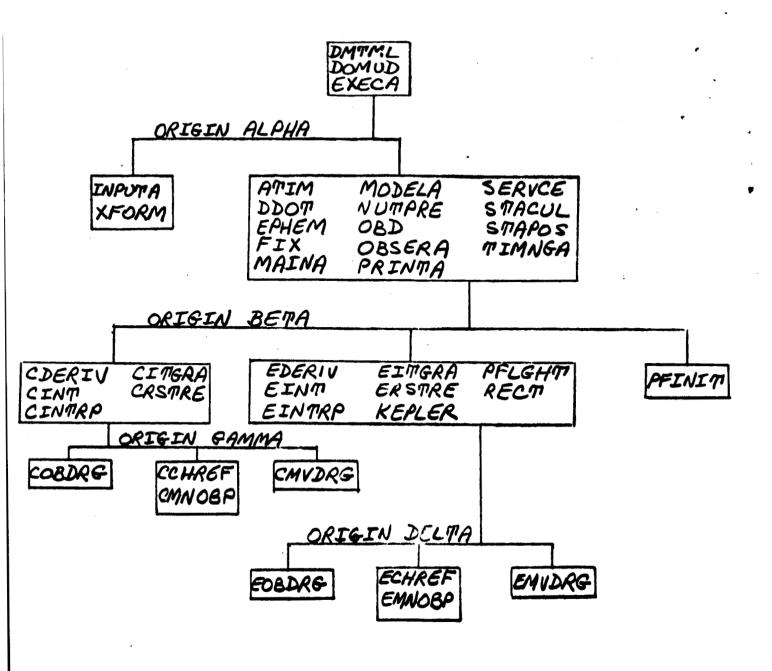


Figure 1
Overlay Structure for Subdivision A

#### 2. GENERAL DESCRIPTION OF INPUT

The Specifications Input is defined as that input which supplies initial conditions, case parameters, station information and control options.

In each of the three program subdivisions (A, Bl, and B2), there is a subroutine whose function is reading the Specifications Input and performing necessary initialization. The names of these subroutines are:

- (a) INPUTA;
- (b) INPTB1;
- (c) B2INPT.

The Specifications Input for each of the three subroutines begins with the reading of a card which contains the major program-defining parameters. The remainder of the input is divided into two groups.

The first group is composed of information which must be specified by the user. Included in this group are such items as launch time, initial vehicle position and velocity, and perturbations to be included in the trajectory computation.

The information in the second group is not necessarily supplied by the user. He can choose to accept a set of values described as standard. If he decides to use standard values, he has the choice of low, intermediate or high precision. Furthermore, he can overwrite as many of these standard values as he wishes. Included in this second group of input values are integration step sizes, the number, type and value of oblateness coefficients to be

used, and the rectification criteria to be used in the run.

Each group of inputs is broken down into several sections.

The first data card of any section to be read must be the section number, in integer format, in columns four and five.

For purposes of stacking cases, the user may choose to bypass any or all sections of the first group except that section which terminates the group. The same applies for the second group with the additional constraint that calling for standard values re-initializes the variables concerned.

The following sections give a detailed description of the input format. The quantity in the description column is entered on the specified card of the section in the appropriate columns. The name given is the name used for the quantity in the program.

# 2.1 INPUT FOR SUBDIVISION A

Sect.	Card	Cols.	<u>Name</u>		
•	1	2-5	KSTDRD	15	40 WILL WANT AT LEAST SOME STANDARD INPUTS
		6-10	MDE	15	>O NO STANDARD. ALL VALUES WILL BE READ IN. =1 TRAJECTORY COMPUTATION =2 OBSERVABLE COMPUTATIONS WITHOUT SIMULATED
					DATA =3 OBSERVABLE COMPUTATIONS WITH SIMULATED DATA
		11-15	PRECIS	F5.0	=4 PREDICTION MODE =1 LOW PRECISION LEVEL =2 INTERMEDIATE PRECISION LEVEL =3 HIGH PRECISION LEVEL
		16-20	CEPID	F5.0	
FIRST	GROUP	OF INPU	TS		
1	1 2	2-72 2-5 6-10	NYEARP DAYS	I5 F5.0	
		21-40	HMIN SEC	F5.0 D20.16	MINUTE OF LAUNCH HOUR SECONDS OF LAUNCH MINUTE
	3	1-24 2-5	TMAX KLM	D24.16 15	TIME OF RUN IN HOURS INDICATOR FOR UNITS OF POSITION AND VFLOCITY VECTOR =1 KM, KM/SEC =2 ER, ER/HR =3 FT, FT/SEC =4 MI, MI/HR = NM, NM/HR
					=6 NM,FT/SEC =7 AU,AU/HR
		6-10	KLML	15	INDICATOR FOR COORDINATE SYSTEM OF INPUT VECTORS =1 CARTESIAN COORD. WE=0 =2 CARTES. COMPUTE WE =3 GEODETIC LONG, LAT, ALT, VE, VN, VH; WE=0 =4 GEODETIC LONG, LAT, ALT, VE, VN, VH; COMPUTE WE =5 GEODETIC LONG, LAT, ALT, V, X, AZ; WE=0 =6 GEODETIC LONG, LAT, ALT, V, X, AZ; COMPUTE WE =7 GEOCENTRIC RA, DECL, ALT, VRA, VD, VH;
					WE=0 =8 GEOCENTRIC RA, DECL, ALT, VRA, VD, VH; COMPUTE WE
					=9 GEOCENTRIC RA, DECL, ALT, V, ,AZ; WE=0
				-10-	=10 GEOCENTRIC RA, DECL, ALT, V, /, AZ;

Sect. Card	Cols.	Name	Type	Description
2 cont.	11-15	KLM2	15	INDICATOR FOR NUTATION AND PRECESSION OF INPUT VECTOR  O NO
	16-20	KSNAP	15	=1 YES INDICATOR FOR NUTATION AND PRECESSION OF VECTORS DURING RUN =0 NO
	21-25	KLM3	15	=1 YES INDICATOR FOR LIBRATION OF INPUT VECTORS =0 NO =1 YES
	26-30	KLIBR	15	INDICATOR FOR LIBRATION OF VECTORS DURING RUN =0 NO =1 YES
	31-35	MRREF	15	INDICATOR FOR INITIAL REFERENCE BODY =1 EARTH =2 SUN =3 MOON =4 MARS =5 VENUS =6 JUPITER =7 SATURN
2	1 <b>-</b> 24 25 <b>-</b> 48	RCIN(1) (2)	D24.16	INITIAL POSITION VECTOR SEE KLM AND KLM1
3	49-72 1-24 25-48 49-72	(3) RDCIN(1) (2) (3)	D24.16 D24.16	
3 1 1		PASFX KS2BY	F5.0 15	TOTAL NUMBER OF PASSES INDICATOR FOR TWO-BODY INTEGRATION ONLY =0 NO =1 YES
	6-10	KSPLT	15	INDICATOR FOR INCLUSION OF PLANETARY PERTURBATIONS =0 NO =1 YES
	11-15	KSOBL	15	INDICATOR FOR INCLUSION OF OBLATENESS PERTURBATION =O NO =1 YES
	16-20	KSDRG	15	INDICATOR FOR INCLUSION OF EARTH DRAG PERTURBATION =O NO
	21#25	KSRAP	15	=1 YES INDICATOR FOR INCLUSION OF RADIATION PRESSURE PERTURBATION =0 NO
	26-30	KSDRGM	15	=1 YES INDICATOR FOR INCLUSION OF MARS DRAG PERTURBATION =0 NO =1 YES

•	Sect. C	and	Cola	Nome	m.	5
-	Dect. U	aru	0013.	<u>Name</u>	<u>Type</u>	<u>Description</u>
	4 cont.		31-35	KSDRGV	15	INDICATOR FOR INCLUSION OF VENUS DRAG PERTURBATION =0 NO
	•		36-40	KSMNOB	15	OBLATENESS PERTURBATION =O NO
			41-45	KRF	15	REFRACTION EFFECTS =O NO
			46-50	KECLPS	15	=1 YES INDICATOR FOR INCLUSION OF ECLIPSE INFO PRINT =0 NO =1 YES
	5 1		2-5	MAXSTA	15	TOTAL NUMBER OF STATIONS USED IN RUN
	2		2-5	K	15	
				STANM(L)	A6	
			20 <b>-30</b>	TYPE(L)	4XI11	
						1.E8*K WHERE A=OBSERVATION TYPES USED BY STATION K IN ASCENDING ORDER L=PACKED STATION NUMBER
	3	•	1-24	STALT(K)	D24.16	LATITUDE OF STATION K
				STALN(K)		LONGITUDE OF STATION K
				STAHT(K)		ALTITUDE OF STATION K
	4		1-36	RRATE(1,L)		(REPETITION RATES (HRS)
	<b>.</b>			RRATE(2,L)		FOR EACH OBSERVATION
	5		1-36	RRATE(3,L) RRATE(4,L)	D36.16 D36.16	TYPE
	6		1-18	TDELAY(1,L)	FIR RV	TIMES IN HRS BEFORE WHICH
	J		19-36	TDELAY(2,L)		EACH OBSERVATION IS NOT
			37-54	TDELAY(3,L)	)	TO BE COMPUTED
			55-72	TDELAY(4,L)	E18.8	
	7		1-18	FUP(K)	E18.8	STA. TRANSMIT FREQ. (MC/S)
			19-36	FDOWN(K)	E18.8	STA. RECEIVE FREQ. (MC/S)
	8		1-24	STAOR(NCDST+1)		CAEE STA. ROTATION ANGLE
			25-48	STAOR (NCDST+2)		AEV STA. ROTATION ANGLE
	9		49-72	STAOR (NCDST+3)	-	(AEN STA. ROTATION ANGLE
	9		1-24 25-48	STAOR(NCDST+4) STAOR(NCDST+5)	D24.16 D24.16	VU STATION LOCATION V ERRORS CAUSED BY
			49-72	STAOR (NCDST+6)	D24.16	W GEODETIC NET ERROR
	10		1-24	STAOR(NCDST+7)	D24.16	NO REFRACTIVITY AT STA.
			25-48	STAOR (NCDST+8)	D24.16	H TROPOSPHERE SCALE FACT
			49-72	STAOR (NCDST+9)	D24.16	PO MAX. ELECTRON DENSITY
	11		1-24	STAOR (NCDST+10)	D24.16	HO LOWER LIMIT OF IONO-
			25-48	STAOR(NCDST+11)	D24.16	HM HT OF PO (KM)
			49-72	STAOR (NCDST+12)	D24.16	-OPEN-
	12.		1-24	STAOR (NCDST+13)	D24.16	AT FOR TIMING
			25-48	STAOR(NCDST+14)	D24.16	BIAS ADDED FOR OBSER.A(1)
	3.0		49-72	STAOR (NCDST+15)	D24.16	BIAS ADDED FOR OBSER.A(2)
	13		1-24	STAOR (NCDST+16)	D24.16	BIAS ADDED FOR OBSER.A(3)
			25-48 Dedeat	STAOR (NCDST+17)	D24.16	BIAS ADDED FOR OBSER.A(4)
		1	REPEAT	CARDS 2-13 FOR EACH	1 STATION -12-	
					<b>- 4</b>	

Sect.	Card	Cols.	Name	Type	<u>Description</u> .
6	1	1-18	DAREAS	E18.8	EFFECTIVE SURFACE AREA OF
		19-36	PAREAS	E18.8	VEHICLE PERTAINING TO DRAG EFFECTIVE SURFACE AREA PERTAINING TO RADIATION PRESSURE
		37-54	SPADD(6)	E18.8	MASS OF VEHICLE
7	1	2-5	MAXLUN	15	MAXIMUM NUMBER OF LUNAR LANDMARKS
		6-10	IPLNT	15	NUMBER OF PLANET TO BE USED FOR
		11 76	TOMAD	<b>T</b> ~	CALCULATING ONBOARD OBSERVATIONS
		11-12	ISTAR	15	NUMBER OF STAR TO BE USED FOR
	2	1 77	ו בו מאשם	/E10 0	CALCULATING ONBOARD OBSERVATIONS
	2	1-72			TABLES NEEDED BY ONBOARD SUBROUTINE
	3	1-72			GIVING POSITIONS OF REFERENCE STARS
	4	1 <b>-</b> 72 ·	STAR(1,9-10) STAR(2,1-2)	4E18.8	AND LANDMARKS. STAR(1,1) AND STAR (2,1) ARE DECLINATION AND RIGHT
	5	1-72	STAR(2,3-6)	<b>∠E</b> 18.8	ASCENSION RESPECTIVELY, OF THE ITH
	6	1-72			STAR. POSLUN(1,1) AND POSLUN(2,1)
	7	1-72			ARE LATITUDE AND LONGITUDE, RESPECT-
	8	1-72	POSLUN(1,5-8)		IVELY, OF THE ITH LANDMARK IN THE
	9	1-72	POSLUN(1,9-10)		LUNAR COORDINATE SYSTEM.
			POSLUN(2,1-2)		1
	10	1-72	POSLUN(2,3-6)		
	11				
8	1	2-5	IUNIT	15	INDICATOR FOR OUTPUT UNITS(SEE KLM)
		6-55	IPSEC(I), I=1,	10 1015	INDICATORS FOR SUPPRESSION OF EACH
	•				OF 10 PRINT SECTIONS
	2	1-18		E18.8	PRINT PORTION (HRS) AND
		19-36	DTSUP	E18.8	SUPPRESS PORTION (HRS), OF TOTAL
	•				PRINT PERIOD
			PRATE	E18.8	INTERVAL WITHIN DTPI AT WHICH TO PHINT
9	1	2-5	NPFSET .	15	NUMBER OF POWERED FLIGHT SETS (UP TO 3)
	2	1-72	PFPAR(1,1-3)	3D24.12	· · · · · · · · · · · · · · · · · · ·
	3		PFPAR(1,4-6)		FY, FZ, MASS.
	Ĺ	1-72	PFPAR(1,7-9)	3D24.12	MASS RATE, T-INTEG, △-PNT
	REPEA		2-4 FOR EACH		

#### 10 END OF FIRST SET OF INPUTS

PROGRAM ADVANCES TO 2ND GROUP OF INPUTS. IF KSTDRD IS NEGATIVE, STANDARD VALUES ARE COMPUTED AND PROGRAM BEGINS TO READ IN 2ND SET OF INPUTS TO CHANGE OR AUGMENT ANY OF THESE STANDARDS. IF KSTDRD NOT NEGATIVE, ALL VALUES ARE READ IN, ELSE VALUES FROM PREVIOUS STACKED CASE ARE USED.

1	1=7	1-72	(DT3(1,J), I=1,3) J=1,7	3D24.12	INTEGRATION INTERVALS FOR EACH OF 7 WORKING BODIES FOR NEAR, MEDIUM AND FAR REFERENCE
2	1	1-72	R1(1-3)	3D24.12	(R1 AND R2 ARE DISTANCES IN
	2			3D24.12	E.R. FOR EACH OF 7 WORKING
	3	1-72	R1(7), $R2(1-2)$	3D24.12 }	BODIES FOR SWITCHING FROM
	4	1-72	R2(3-5)	3D24.12	NEAR TO MEDIUM AND MEDIUM TO
	5	1-48	R2(6-7)	2D24.12)	(FAR INTEGRATION INTERVALS.

Sect.	Card	Cols.	Name_	Type	Description
3.	1	1-24		D24.12}	VALUES USED AS TOLERANCES IN
	_	25-48		D24.12.	RECTIFICATION CRITERIA
•4	1	1-18	DHI	E18.8	TROPOSPHERE INTEGRATION STEP SIZE (KM)
•		19-36		E18.8	IONOSPHERE INTEGRATION STEP SIZE (KM)
		37-54	H2	E18.8	UPPER LIMIT TROPOSPHERE (KM)
		55-72		E18.8	UPPER LIMIT IONOSPHERE (KM)
5	1	-	KOBLAT	15	NUMBER OF OBLATENESS COEFFS
	2	2-5		15	M INDEX
		6-10		I5	N INDEX
		11-15	ISORC	15 )	INDICATOR FOR C OR S COEFF.
				÷	=0 S
		_		ز <b>ح. ح</b> .	(=1 C
	3	1-24		D24.12	VALUE OF COEFFICIENT
	REP	EAT CAR	DS 2-3 UNTIL KO	BLAT VALUES F	HAVE BEEN READ IN.
6	1	2-5	MBMAX	15	NUMBER OF WORKING BODIES
Ū	-	6	KWBMU(I).	-	INDICES OF WORKING BODIES
			I=1,MBMAX(MBMA	XX)* 35	
	2	1-72	TPMAT8(1),	3D24.12	GRAVITATIONAL CONSTANTS OF WORKING
			I=1,MBMAX		BODIES
	REP	EAT CAR	D 2 FOR EACH VA	ALUE OVER 3N 1	NEEDED
7	1	1-24	DYN(48)	D24.12	SOLAR FLUX
		25–48	DYN(49)	D24.12	CPEN
8	1		DYN(51-53)		
9	1 .		COMB(I)	D24.12	VELOCITY OF LIGHT
10	1	1-72	PRNT3(1-3)	3D24.12	PRINT INTERVALS(HRS) FOR NEAR MEDIUM AND FAR REFERENCE
11	1	1-24	EMIN	D24.12	MINIMUM VALUE OF ELEVATION ANGLE(RAD)
12	1	1-18	RTO	E18.8	RATIO OF NORDSIECK INTEGRATION
					INTERVAL TO THAT IN RUNGE-KUTTA
13	1	1-24	DSPL	D24.12	SPECIAL INTEGRATION INTERVAL IN A4
					MODE TO OBTAIN ACQUISITION TIME
			, ,	<b>-</b>	(HRS)
14	1	1-72	RATEV(1-3,1)	3D24.12	ROTATION VECTOR USED IN MARS DRAG
			,		COMPUTATIONS
	2	1-72	RATEV(1-3,2)	3D24.12	ROTATION VECTOR USED IN VENUS DRAG
					COMPUTATIONS
15	1-10	1-72	XMACH(I),	4E18.8	MACH NUMBER TABLE
			I=1,40		AND A CONTRACTION BANKS
	11-20	1-72	CDT(I),	4E18.8	DRAG COEFFICIENT TABLE
- 4			I=1,40	<b>-20 -</b>	MOT NO ANOTHER TOP COMMERCENTIANS OF STREET
16	1	1-20	SPADD(7)	E20.8	TOLERANCE FOR CONVERGENCE OF NEWTON-
					RAPHSON SCHEME IN OCCULTATION SUB-
					ROUTI NE
		21-25	IXADD(15)	15	MAXIMUM NUMBER OF NEWTON-RAPHSON ITERATIONS IN OCCULTATION SUBROUTINE

Sect.	Card	Cols.	<u>Name</u>	Type	Description
		26-30	IXADD(16)	15	FLAG FOR OCCULTATION O, DO NOT CONSIDER O, STAR OCCULTATION O, NUMBER OF FIRST STATION FOR VEHICLE OCCULTATION
		31-35 36-40 41-45	IXADD(17) IXADD(18) IXADD(20)	15 15 15	NUMBER OF SECOND STATION NUMBER OF THIRD STATION NUMBER OF STATIONS TO BE CONSIDERED
17 18 19	ENT) (	OPEN OPEN OF 2ND O	ROUP OF INPUTS		:

# 2.2 INPUT FOR SUBDIVISION B1

Sect.	Card	Cols.	<u>Name</u>	Type	<u>Description</u>
•	. 1	2-5	KSTDRD	15	<pre>&lt;0 WILL WANT AT LEAST SOME STANDARD INPUTS. ≥0 NO STANDARD. ALL VALUES WILL BE READ IN.</pre>
•		6–10	IMODE	15	=1 REAL DATA =2 SIMULATED DATA =3 ERROR ANALYSIS =4 PRELIMINARY SCAN =5 PROPAGATION OF ERRORS =6 MISS COEFFICIENTS
		11-15	PRECIS	F5.0	=1 LOW PRECISION LEVEL =2 INTERMEDIATE PRECISION LEVEL =3 HIGH PRECISION LEVEL
		16–20	CEPID	F5.0	=0,1 ENCKE INTEGRATION =-1 COWELL INTEGRATION
		21-25	ISUMRY	15	=0 NO SUMMARY =1 SUMMARY
		26–30	ISTAT	15	=0 MINIMUM VARIANCE =1 LEAST SQUARES
FIRST G	ROUP OF	INPUTS			
1	1 2	2-72 2-5 6-10 11-15 16-20	ITITLE(1-12) NYEARP DAYS HRS HMIN	12A6 15 F5.0 F5.0 F5.0	TITLE YEAR OF LAUNCH DAY OF LAUNCH YEAR HOUR OF LAUNCH DAY MINUTE OF LAUNCH HOUR SECONDS OF LAUNCH MINUTE
2	3	21-40 1-24 2-5	SEC TMAX KLM	D20.16 D24.12 I5	TIME OF RUN IN HOURS INDICATOR FOR UNITS OF POSITION AND VELOCITY VECTOR =1 KM, KM/SEC =2 ER, ER/HR =3 FT, FT/SEC =4 MI, MI/HR =5 NM, NM/HR =6 NM, FT/SEC =7 AU, AU/HR
		6-10	KLM1	I5	INDICATOR FOR COORDINATE SYSTEM OF INPUT VECTORS  =1 CARTESIAN COORD. WE=0  =2 CARTES. COMPUTE WE  =3 GEODETIC LONG, LAT, ALT VE, VN, VH; WE =0  =4 GEODETIC LONG, LAT, ALT VE, VN, VH; COMPUTE WE  =5 GEODETIC LONG, LAT, ALT  V , X, AZ; WE =0  =6 GEODETIC LONG, LAT, ALT  V , X, AZ; COMPUTE WE

Sect.	Card	Cols.	Name	<u>Type</u>	Description
,					=7 GEOCENTRIC RA, DECL, ALT VRA, VD ,VH; WE=0 .
					=8 GEOCENTRIC RA, DECL, ALT VRA, VD, VH; COMPUTE WE
					=9 GEOCENTRIC RA, DECL, ALT  V , X, AZ; WE=0 =10 GEOCENTRIC RA, DECL, ALT
		11-15	KLM2	15	INDICATOR FOR NUTATION AND PRE-
					CESSION OF INPUT VECTOR = 0 NO
		16-20	KSNAP	15	=1 YES INDICATOR FOR NUTATION AND PRE- CESSION OF VECTORS DURING RUN
				_	=O NO =1 YES
		21-25	KLM3	15	INDICATOR FOR LIBRATION OF INPUT VECTORS =0 NO =1 YES
		26-30	KLIBR	15	INDICATOR FOR LIBRATION OF VECTORS DURING RUN =0 NO
		31-35	MRREF	15	=1 YES INDICATOR FOR INITIAL REFERENCE
					BODY =1 EARTH
					=2 SUN =3 MOON =4 MARS
					=5 VENUS =6 JUPITER =7 SATURN
	2	1-24 25-48	RCIN(1) (2)	D24.16 D24.16	INITIAL POSITION VECTOR (VALUES DEPEND ON KLM1 AND
	3	49-79 1-24	(3) RDCIN(1)	D24.16 D24.16	<pre>{ KLM) {INITIAL VELOCITY VECTOR } (VALUES DEPEND ON KLM1 AND</pre>
3	1	25-48 49-72 2-5	(2) (3) IQZERO	D24.16 D24.16 I5	( KLM) =O USE INPUT Q MATRIX
	_	6-10	PASFX	F5.0	=1 USE GROWN Q MATRIX TOTAL NUMBER OF PASSES (1)
		11 <b>-</b> 15 16-39	PASS2 TMAX2	F5.0 D24.16	TOTAL NUMBER OF PASSES (2) TIME OF RUN FOR 2ND GROUP
4	1	2-5	KS2BY	15	INDICATOR FOR TWO-BODY ONLY =O NO
		6-10	KSPLT	15	=1 YES INDICATOR FOR INCLUSION OF PLANETARY PERTURBATIONS =0 NO =1 YES

Sect	Card	Cols.	Name	Type	Description
•		11-15	KSOBL	15	INDICATOR FOR INCLUSION OF OBLATENESS PERTURBATION =O NO =1 YES
		16-20	KSDRG	15	INDICATOR FOR INCLUSION OF EARTH DRAG PERTURBATION =0 NO =1 YES
·		21-25	KSRAP	15	INDICATOR FOR INCLUSION OF RADIA- TION PRESSURE PERTURBATION =0 NO =1 YES
		26–30	KSDRGM	15	INDICATOR FOR INCLUSION OF MARS DRAG PERTURBATION =0 NO =1 YES
		31-35	KSDRGV	15	INDICATOR FOR INCLUSION OF VENUS DRAG PERTURBATION =0 NO =1 YES
		36-40	KSMNOB	15	INDICATOR FOR INCLUSION OF MOON OBLATENESS PERTURBATION =0 NO =1 YES
·		41-45	KRF	15	INDICATOR FOR INCLUSION OF REFRAC- TION EFFECTS =0 NO =1 YES
		46-50	KECLPS	15	INDICATOR FOR INCLUSION OF ECLIPSE INFO PRINT =0 NO =1 YES
		51-55	KTC	15	INDICATOR FOR INCLUSION OF TIME CORRECTION =0 NO =1 YES
		56 <b>–6</b> 0	IRDATA	I5	INDICATOR FOR DATA REJECTION =0 NO =1 YES
5	1	2-5	MAXSTA	15	TOTAL NUMBER OF STATIONS USED IN RUN
	2	2-5 10-15 20-30	K STANM(K) TYPE(K)	15 4XA6 4XI11	STATION NUMBER  STATION NAME  A(1)/1.E2*A(2)/1.E4*A(3)/ 1.E6*A(4)/1.E8*K WHERE  A= OBSERVATION TYPES USED BY  STATION K IN ASCENDING ORDER
:	3	1-24 25-48 49-72	STALT(K) STALN(K) STAHT(K)	D24.16 D24.16 D24.16	LATITUDE OF STATION K LONGITUDE OF STATION K ALTITUDE OF STATION K
	4	5-15	STATYP(K)	4XI11	ALL OBSERVATION TYPES THE STATION CAN MEASURE (SAME FORMAT AS TYPE (K)

					•
İ	5	1-18	TDELAY(1,K)	E18.87	( TIMES IN HRS, BEFORE WHICH
		19-36	TDELAY (2,K)	E18.8 }	EACH OBSERVATION IS NOT
		37-54	TDELAY (3,K)	E18.8 \	TO BE COMPUTED.
		55 <b>-</b> 72	TDELAY(4,K)	E18.8	10 22 00.11 01.22
1	6	1-18	FUP(K)	E18.8	STA. TRANSMIT. FREQ. (MC/3)
	O	19-36	FDOWN(K)	E18.8	STA. RECEIVE FREQ. (MC/3)
,	7		STAOR(NCDST/1)		CEEN (STA. ROTATION ANGLE
		1-24		D24.16	
		25-48	STAOR(NCDST/2)	D24.16	△EV/STA. ROTATION ANGLE
Ì		49-72	STAOR(NCDST/3)	D24.16	(AEN STA. ROTATION ANGLE
	8	1-24	STAOR(NCDST/4)	D24.16	U STATION LOCATION
		25-48	STAOR(NCDST/5)	D24.16	V ERRORS CAUSED BY
		49-72	stagr(ncdst/6)	D24.16	GEODETIC NET ERROR
İ	9	1-24	STAOR(NCDST/7)	D24.16	NO REFRACTIVITY AT STA.
		25-48	STAOR(NCDST/8)	D24.16	H TROPOSPHERE SCALE FACT
		49-72	STAOR(NCDST/9)	D24.16	PO MAX. ELECTRON DENSITY
	10	1-24	STAOR(NCDST/10)	D24.16	HO LOWER LIMIT OF IONCSPHERE (KM)
		25-48	STAOR(NCDST/11)	D24.16	HM HT OF PO (KM)
1		49-72	STAOR(NCDST/12)	D24.16	-OPEN-
	11	1-24	STAOR(NCDST/13)	D24.16	AT FOR TIMING
		25-48	STAOR(NCDST/14)	D24.16	BIAS ADDED FOR OBSER.A(1)
		49-72	STAOR(NCDST/15)	D24.16	BIAS ADDED FOR OBSER.A(2)
	12	1-24	STAOR(NCDST/16)	D24.16	BIAS ADDED FOR OBSER.A(3)
	-~	25-48	STAUR(NCDST/17)	D24.16	BIAS ADDED FOR OBSER.A(4)
	13	1-72	TEBAR(1,J,K),	4E18.8)	COVARIANCE MATRIX
1	.دی	1-12	J=1,4	1 0.01	)
	14	1-72	TEBAR(2,J,K),	4E18.8	FOR STATION K
	14	1-12	* -	4610.0	C FOR STATION R
	15	1-72	J=1,4 TEBAR(3,J,K),	/F10 0	
	15	1-72		4E18.8	
	14	7 770	J=1,4	(Find d	
	16	1-72	TEBAR(4,J,K),	4E18.8)	
			J=1,4	•	
		AN MAGGG	DOS O 14 FOR FACE CO	AMTON	
		REFERI CA.	RDS 2-16 FOR EACH ST	ATION.	
6	1	1-18	DAREAS	E18.8	EFFECTIVE SURFACE AREA OF VEHICLE
				-	PERTAINING TO DRAG
		19-36	PAREAS	E18.8	EFFECTIVE SURFACE AREA PERTAINING
1					TO RADIATION PRESSURE
		37-54	SPADD(6)	E18.8	MASS OF VEHICLE
7	1	2-5	MAXLUN	I5	MAXIMUM NUMBER OF LUNAR LANDMARKS
		6-10	IPLNT	Ī5	NUMBER OF PLANET TO BE USED FOR
		0 10		<b>-</b> )	CALCULATING ONBOARD OBSERVATIONS .
		11-15	ISTAR	15	NUMBER OF STAR TO BE USED FOR
		11 1)	202111	<b>1</b> )	CALCULATING ONBOARD OBSERVATIONS
	2	1-72	STAR(1,1-4)	4E18.8	TABLES NEEDED BY ON-BOARD
	3	1-72	STAR(1,5-8)	•	SUBROUTINE GIVING POSITIONS OF
				4E18.8	REFERENCE STARS AND LANDMARKS.
	4	1–72	STAR(1,9-10),	4E18.8	<del></del>
	r	1 770	STAR(2,1-2)	(Dad d	STAR(1,I) AND STAR(2,I) ARE DE-
	5	1-72	STAR(2,3-6)	4E18.8	CLINATION AND RIGHT ASCENSION,
	6	1-72	STAR(2,7-10)	4E18.8	RESPECTIVELY, OF THE ITH STAR.
	7	1-72	POSLUN(1,1-4)	4E18.8	POSLUN (1,1) AND POSLUN (2,1) ARE
	8	1-72	POSLUN(1,5-8)	4E18.8	LATITUDE AND LONGITUDE, RESPECTIVELY,
	9	1-72	POSLUN(1,9-10),	4E18.8	OF THE LANDMARK IN THE LUNAR COOR-
			POSLUN(2,1-2)		dinate system.
				-19-	

<u>Type</u>

Description

Card

Sect.

Cols.

Name

Sect.	Card	Cols.	<u>Name</u>	Type	Description
	10	1-72	POSLUN(2,3-6)	4E18.8	
•	11	1-72	POSLUN(2,7-10)	4E18.8	
8	. 1	2-5	IUNIT	15	INDICATOR FOR OUTPUT UNITS (SEE KLM)
•		6-10	KOPT	15	INDICATOR OF DESIRED OPTION OF KSECPR ARRAY FOR PRINTING STATIS- TICS
		11–60	IPSEC(I), I= 1,10	1015	INDICATORS FOR SUPPRESSION OF EACH OF 10 PRINT SECTIONS
	2	1-18	DTPI	E18.8	PRINT PORTION (HRS) OF )
	~	19-36	DTSUP	E18.8	SUPPRESS PORTION (HRS) OF TOTAL
		מת בו	PRATE	wad d	PRINT PERIOD INDICATOR FOR USE OF ABOVE PRINT
		37-54	PRAIE	E18.8	PERIOD
	3	1-24	DTP	D24.12	INCREMENT FOR PRINT TIME
9	1	2-5	NPFSET	15	NUMBER OF POWERED FLIGHT JETS (UP TO 3)
	2	1-72	PFPAR(I,1-3)	3D24.12	
	3	1-72	PFPAR(1,4-6)	3D24.12	
	4	1-72	PFPAR(1,7-9)	3D24.12	MASS RATE, AT-INTEG, A-PNT
	4	1-12	111 RM(1) (-7)	)D 24.12	THOS INTEGRAL THIRD , WITH THE
		REPEAT CARI	OS 2-4 FOR EACH I WI	HERE I=1, NI	PFSET
10	1	2-5	MAXSTA	15	NUMBER OF STATIONS USED
	2	2-5	KSTA	15	STATION NUMBER
		6-25	KM(I), I=1,4	415	FREQUENCY OF ACCEPTANCE OF DATA TYPES
	3	1-72	EBRMLT(J,KSTA), J=1,4	4E18.8	ARRAY OF EBAR MATRIX MULTIPLIERS
		REPEAT CARI	OS 2-3 FOR EACH STA	TION	
11	1	1-5	NOFT	15	NUMBER OF TIMES THROUGH BAYES FOR CONVERGENCE
		6-10	MXPASS	I5	MAXIMUM VALUE OF PASS COUNTER
	2	1-24	TOLSQ	D24.16	SQUARE OF TOLERANCE FOR CONVERGENCE
	~	25-48	TPREIM	D24.16	MAX. TIME OF PRELIMINARY BATCH
	3	1-72	TSPAN(1-3)	3D24.16?	(TIME SPAN OF EACH BATCH
	3 4	1-72	TSPAN (4-6)	3D24.16	I DIAN OF MADE EATOR
12	1	2-5	IPMAT	I5	INDICATOR FOR MATRIX INPUT
	1	<b>.</b> -y	11161	-,	=0 P MATRIX TO BE READ IN =1 Q MATRIX TO BE READ IN
	2-13	1-72	(QSAVE(I,J),J=	3D24.12	P OR Q MATRIX DEPENDING ON IPMAT
	~ 1)		1,6),I=1,6)	J~ ~~+ + ± ~	- car & married but modern on third
-13		-OPEN-			
14		-OPEN-			
15		-OPEN-			
16		-OPEN-			
17		-OPEN-			
18		-OPEN-			

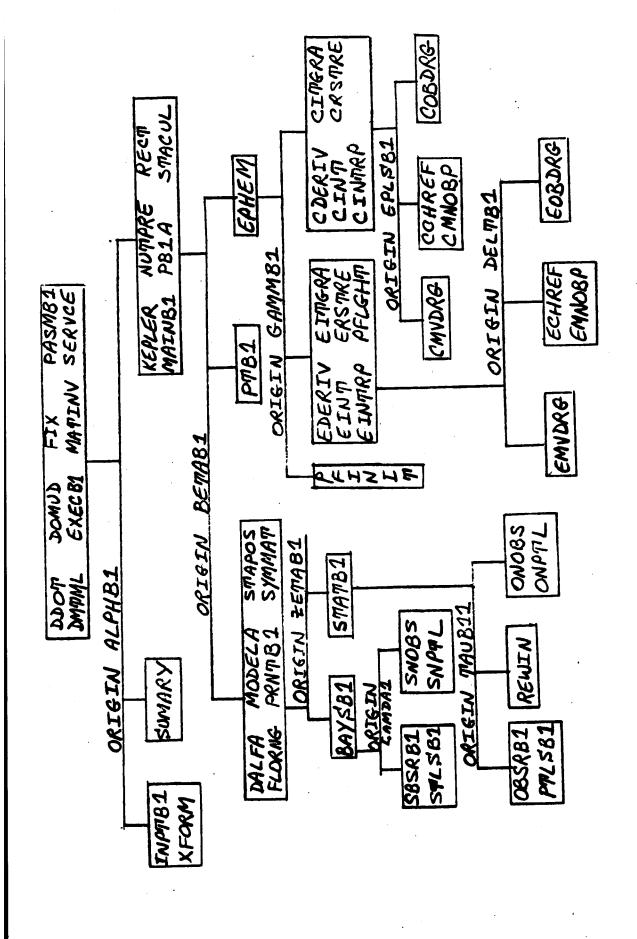


Figure 2

Overlay Structure for Subdivision Bl

Sect.	Card	Cols.	Name	Type	<u>Description</u>
19 20 •		-OPEN- END OF FI	RST SET OF INPU	<b>T</b> S	

PROGRAM ADVANCES TO 2ND GROUP OF INPUTS. IF KSTDRD IS NEGATIVE, STANDARD VALUES ARE COMPUTED AND PROGRAM BEGINS TO READ IN 2ND SET OF INPUTS TO CHANGE OR AUGMENT ANY OF THESE STANDARDS. IF KSTDRD NOT NEGATIVE, ALL VALUES ARE READ IN, ELSE VALUES FROM PREVIOUS STACKED CASE ARE USED.

SIHOKED	CASE AR	മ ധാമം.			
1	1-7	1-72	(DT3(I,J),I= 1,3),J=1,7	3D24.12	INTEGRATION INTERVALS FOR EACH OF 7 WORKING BODIES FOR NEAR, MEDIUM AND FAR REFERENCE
2	1	1-72	R1(1-3)	3D24.12)	R1 and R2 ARE DISTANCES IN
	2	1-72		3D2/-12	E.R. FOR EACH OF 7 WORKING
	2 3	1-72		3D2/_12	BODIES FOR SWITCHING FROM
	4	1-72		3D24.12	NEAR TO MEDIUM AND MEDIUM TO
	5		R2(6-7)		FAR INTEGRATION INTERVALS.
3	í	1-24	RT1		VALUES USED AS TOLERANCES IN
	-	25-48			RECTIFICATION CRITERIA
4	1	1-18		E18.8	TROPOSPHERE INTEGRATION STEP
*	+	1-10	2111	210.0	SIZE (KM)
		19-36	DH2	E18.8	IONOSPHERE INTEGRATION STEP
		1, 50	2112		()
		37-54	H2	E18.8	UPPER LIMIT TROPOSPHERE(KM)
				E18.8	UPPER LIMIT IONOSPHERE(KM)
<b>r</b> ,	1	2-5	H4 KOBLAT	15	NUMBER OF OBLATENESS COEFFS.
	2	2-5	M	ĪŚ	M INDEX
		2-5 6-10	N	<b>1</b> 5	N INDEX
		11-15	1SORC	ĪŚ	UPPER LIMIT TROPOSPHERE(KM) UPPER LIMIT IONOSPHERE(KM) NUMBER OF OBLATENESS COEFFS. M INDEX N INDEX INDICATOR FOR C OR S COEFF.
				•	=0 3
			·		=1 C
	3	1-24	SORCCF	D24.12	VALUE OF COEFFICIENT
		REPEAT CAR	DS 2-3 UNTIL KOBL	AT VALUES HAVE	BEEN READ IN.
6	1	2-5	MBMAX	15	NUMBER OF WORKING BODIES
		6-	KWBMU(I), I=1,		INDICES OF WORKING BODIES
			MBMAX	(MBMAK)*15	
	2	1-72	TPMAT8(I),I=1, MBMAX	3D24.12	GRAVITATIONAL CONSTANTS OF WORKING BODIES
		REPEAT CAR	D 2 FOR EACH VALU	e over 3n need	ED
7	1	1-24	DYN(48)	D24.12	SOLAR FLUX
		25-48	DYN (49)	D24.12	OPEN
8	1	1-72	DYN(51-53)	3D24.12	COEFFS. FOR LUNAR OBLATENESS
9	1	1-24	COMB(1)	D24.12	VELOCITY OF LIGHT
10	1	1-72	PRNT3(1-3)	3D24.12	PRINT INTERVALS (HRS) FOR NEAR MEDIUM AND FAR REFERENCE
11	1	1-24	EMIN	D24.12	MINIMUM ELEVATION ANGLE (RAD)
12	i	1-18	RTO	E18.8	RATIO OF NORDSIECK INTEGRATION
-~	•	1-10	1110	210.0	INTERVAL TO THAT IN RUNGE-KUTTA

Sect.	Card	Cols.	<u>Name</u>	<u>Type</u>	<u>Description</u>
13		-OPEN-			•
14	1	1-72	RATEV(1-3,1)	3D24.12	ROTATION VECTOR USED IN MARS DRAG COMPUTATIONS
	2	1-72	RATEV(1-3,2)	3D24.12	ROTATION VECTOR USED IN VENUS DRAG COMPUTATIONS
15	1-10 11-20	1 <b>-</b> 72 1 <b>-</b> 72	XMACH(I),I=1,40 CDT(I),I=1,40	4E18.8 4E18.8	MACH NUMBER TABLE DRAG COEFFICIENT TABLE
16	1 2	1-72 1-72	DELX(I),I=1,3 DELX(I),I=4,6	3D24.16 3D24.16	STATE VARIABLES
17	1	1 <b>-</b> 18 19-36	REJCT1 REJCT2	E18.8 }	NUMBER OF STANDARD DEVIATIONS ABOVE WHICH DATA ARE REJECTED ON FIRST AND SUBSEQUENT PASSES, RE- SPECTIVELY
18		-OPEN-			_
19	TMD 071	-OPEN-	OF INDIFFE		
20	END OF 2	2ND GROUP	OF INPUTS	1	

2.3	INPUT F	OR SUBDIV	1510N B2		
Sect:	Card	Cols.	Name	Type	<u>Description</u>
	1	2-5	KSTDRD	15	✓ O WILL WANT AT LEAST SOME STANDARD INPUTS ➢ O NO STANDARD. ALL VALUES WILL BE READ IN.
		6-10	IMODE	15	=1 REAL DATA =2 SIMULATED DATA =3 ERROR ANALYSIS =4 PRELIMINARY SCAN =5 PROPAGATION OF ERRORS =6 MISS COEFFICIENTS
		11-15	PRECIS	F5.0	=1 LOW PRECISION LEVEL =2 INTERMEDIATE PRECISION LEVEL =3 HIGH PRECISION LEVEL
		16-20	CEPID	F5.0	=0,1 ENCKE INTEGRATION =-1 COWELL INTEGRATION
		21-25	ISUMRY	15	=O NO SUMMARY =1 SUMMARY
		26-30	ISTAT	15	= O MINIMUM VARIANCE = 1 LEAST SQUARES
FIRST	GROUP OF	TNPHTS			
			ITITIE(1-	12) 12A6	TITIE
					YEAR OF LAUNCH
		6-10	DAYS	F5.0	DAY OF LAUNCH YEAR
		11-15	HRS	F5.0	HOUR OF LAUNCH DAY
		16-20	HMIN	F5.0	MINUTE OF LAUNCH HOUR
		21-40	SEC	D20.16	SECONDS OF LAUNCH MINUTE
	3	1-24	TMAX	D24.12	TIME OF RUN IN HOURS
2	1	2-5	KL M	15	INDICATOR FOR UNITS OF POSITION AND VELOCITY VECTOR =1 KM.KM/SEC =2 ER. ER/HR =3 FT.FT/SEC =4 MI.MI/HR =5 NM.NM/HR =6 NM.FT/SEC =7 AU.AU/HR

2.3 Cont'	2 .	. 3		C	٥	n	t	•	1
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Sect.	Card	Cols.	Name	Type	Description
		6-10	KLM1	15	INDICATOR FOR COORDINATE SYSTEM OF INPUT VECTORS  =1 CARTESIAN COORD. WE=0  =2 CARTES. COMPUTE WE  =3 GEODETIC LONG, LAT, ALT     VE, VN, VH; WE =0  =4 GEODETIC LONG, LAT, ALT     VE, VN, VH; COMPUTE WE  =5 GEODETIC LONG, LAT, ALT      V , 0, AZ; WE=0  =6 GEODETIC LONG, LAT, ALT      V , 0, AZ; COMPUTE WE  =7 GEOCENTRIC RA, DECL, ALT     VRA, VD, VH; WE=0  =8 GEOCENTRIC RA, DECL, ALT      VRA, VD, VH; COMPUTE WE  =9 GEOCENTRIC RA, DECL, ALT      V , 0, AZ; WE=0  =10 GEOCENTRIC RA, DECL, AL
	·	11-15	KI M2	15	INDICATOR FOR NUTATION AND PRECESSION OF INPUT VECTOR = 0 NO = 1 YES
		16-20	KSNAP	15	INDICATOR FOR NUTATION AND PRECESSION OF VECTORS DURING RUN = 0 NO = 1 YES
		21-25	KL M3	15	INDICATOR FOR LIBRATION OF INPUT VECTORS = 0 NO = 1 YES
		26-30	KLIBR	15	INDICATOR FOR LIBRATION OF VECTORS DURING RUN =0 NO =1 YES
		31-35	MRREF	15	INDICATOR FOR INITIAL REFERENCE BODY =1 EARTH =2 SUN =3 MOON =4 MARS =5 VENUS =6 JUPITER =7 SATURN

2	. 3	(	•	0	n	t.	٠	d

=:=					
Sect.	Card	Cols.	Name	Type	Description
	2	1-24	RCIN(1)	D24.16/	(INITIAL POSITION VECTOR
•		25-48	(2)	D24.16	(VALUES DEPEND ON
		49-79	(3)	D24.16)	KLM1 AND KLM)
	3	1-24	RDCIN(1)	D24.16	INITIAL VELOCITY VECTOR
		25-48	(2)	D24.16	(VALUES DEPEND ON
		49-72	(3)	D24.16/	KIMI AND KLM)
3	1	2-5	IQZERO	I 5	= O USE INPUT Q MATRIX = 1 USE GROWN Q MATRIX
		6-10	PASFX	F5.0	TOTAL NUMBER OF PASSES (1)
		11-15	PASS2	F5.0	TOTAL NUMBER OF PASSES (2)
		16-39	TMAX2	D24.16	TIME OF RUN FOR 2nd GROUP
4	1	2-5	KS2BY	15	INDICATOR FOR TWO-BODY ONLY
		:		•	=O NO =1 YES
		6-10	KSPLT	15	INDICATOR FOR INCLUSION OF PLANETARY PERTURBATIONS = 0 NO = 1 YES
		11-15	KS OB L	15	INDICATOR FOR INCLUSION OF OBLATENESS PERTURBATION = 0 NO = 1 YES
		16-20	KSDRG	15	INDICATOR FOR INCLUSION OF EARTH DRAG PERTURBATION = 0 NO = 1 YES
		21-25	KSRAP	15	INDICATOR FOR INCLUSION OF RADIATION PRESSURE PERTURB. =0 NO =1 YES
		26-30	KSDRGM	15	INDICATOR FOR INCLUSION OF MARS DRAG PERTURBATION = 0 NO = 1 YES

2.3 Cont'd

Sect	Card	Cols.	Name	Type	Description
		31-35	KSDRGV	r <b>5</b>	INDICATOR FOR INCLUSION OF VENUS DRAG PERTURBATION = 0 NO = 1 YES
		36-40	KSMNOB	15	INDICATOR FOR INCLUSION OF MOON OBLATENESS PERTURBAT. = 0 NO = 1 YES
		41-45	KRF	15	INDICATOR FOR INCLUSION OF REFRACTION EFFECTS: =0 NO =1 YES
		46-50	KECLPS	I <b>5</b>	INDICATOR FOR INCLUSION OF ECLIPSE INFO PRINT = 0 NO = 1 YES
		51-55	KTC	15	INDICATOR FOR INCLUSION OF TIME CORRECTION = 0 NO = 1 YES
		56-60	IRDATA	15	INDICATOR FOR DATA REJECTION =0 NO =1 YES
5	1	2-5	MAXSTA	15	TOTAL NUMBER OF STATIONS USED IN RUN
	2	2-5	K	15	STATION NUMBER
		10-15	STANM(K)	4XA6	STATION NAME
		20-30	TYPE(K)	<b>4X</b> 111	A(1)+1.E2*A(2)+1.E4*A(3)+ 1.E6*A(4)+1.E8*K WHERE A= OBSERVATION TYPES USED BY STATION K IN ASCENDING ORDER
	3	1-24	STALT (K)	D24.16	LATITUDE OF STATION K
		25-48	STALN(K)	D24.16	LONGITUDE OF STATION K
		49-72	STAHT (K)	D24.16	ALTITUDE OF STATION K
	4	5-15	STATYP(K)	4X111	ALL OBSERVATION TYPES THE STATION CAN MEASURE (SAME FORMAT AS TYPE(K))

# 2.3 Cont'd

Sect.	Card	Cols.	<u>Name</u>	Type	Description
•	5	1-18	TDELAY(1,K)	E18.8)	TIMES IN HRS.
		19-36	TDELAY(2,K)	E18.8	BEFORE
	•	37-54	TDELAY(3,K)	E18.8	EACH OBSERVATION
		55-72	TDELAY(4,K)	E18.8	IS NOT TO BE COMPUTED
_			·	J 1	<b>'</b> .
	6	1-18	FUP(K)	E18.8	STA. TRANSMIT. FREQ. (MS/S)
		19-36	FDOWN(K)	E18.8	STA. RECEIV. FREQ. (MC/S)
	7	1-24	STAOR (NCDST+1)	D24.16	AEE STA. ROTATION ANGLE
		25-48	STAOR (NCDST+2)	D24.16	SEV STA. ROTATION ANGLE
		49-72	STAOR (NCDST+3)	D24.16	AEN STA. ROTATION ANGLE
	8	1-24	STAOR (NCDST+4)	D24.16 A	LU STATION LOCATION
		25-48	STAOR (NCDST+5	D24.16 L	ERRORS V CAUSED
		49-72	STAOR (NCDST+6)	D24.16 Z	BY W GEODETIC NET ERROR
	9	1-24	STAOR (NCDST+7)	D24.16	NO REFRACTIVITY AT STA.
		25-48	STAOR (NCDST+8)	D24.16	H TROPOSPHERE SCALE FACT
		49-72	STAOR (NCDST+9)	D24.16	PO MAX. ELECTRON DENSITY
	10	1-24	STAOR (NCDST+10)	D24.16	HO LOWER LIMIT OF IONOSPHERE
		25-48	STAOR (NCDST+11)	D24.16	HM HT OF PO (KM)
		49-72	STAOR (NCDST+12)	D24.16	-OPEN-
	11	1-24	STAOR (NCDST+13)	D24.16	AT FOR TIMING
,		25-48	STAOR (NCDST+14)	D24.16	BIAS ADDED FOR OBSER.A(1)
		49-72	STAOR (NCDST+15)	D24.16	BIAS ADDED FOR OBSER.A(2)
	12	1-24	STAOR (NCDST+16)	D24.16	BIAS ADDED FOR OBSER.A(3)
		25-48	STAOR (NCDST+17)	D24.16	BIAS ADDED FOR OBSER.A(4)
	13	1-72	TEBAR(1, J, K), J=1,	4 4E18.8	COVARIANCE MATRIX
	14	1-72	TEBAR(2, J, K), J=1,	4 4E18.8	FOR
	15	1-72	TEBAR $(3, J, K), J=1$ ,	4 4E18.8	STATION
	16	1-72 RE	TEBAR(4,J,K) J=1, PEAT CARDS 2-16 FO	-	

# 2.3 Cont'd

Sect.	Card	Cols.	Name	Type	<u>Description</u>
6	1	1-18	DAREAS	E18.8	EFFECTIVE SURFACE AREA OF VEHICLE PERTAINING TO DRAG
		19-36	PAREAS	E18.8	EFFECTIVE SURFACE AREA PERTAINING TO RADIATION PRESSURE
		37-54	SPADD(6)	E18.8	MASS OF VEHICLE
7	1	2-5	MAXLUN	15	MAXIMUM NUMBER OF LUNAR LANDMARKS
		6-10	I PL.NT	15	NUMBER OF PLANET TO BE USED FOR CALCULATING ONBOARD OBSERVATIONS
		11-15	ISTAR	<b>I5</b> :	NUMBER OF STAR TO BE USED FOR CALCULATING ONBOARD OBSERVATIONS
	2	1-72	STAR(1,1-4)	4E18.8	TABLES NEEDED BY ON-BOARD
	3	1-72	STAR(1,5-8)	4E18.8	SUBROUTINE GIVING POSITIONS
	4	1-72	STAR(1,9-10), STAR(2,1-2)	4E18.8	OF REFERENCE STARS AND LANDMARKS, STAR (1,1) (AND
	5	1-72	STAR(2,3-6)	4E18.8	ISTAR (2,1)
	6	1-72	STAR(2,7-10)	4E18.8	RIGHT ASCENSION
	7	1-72	POSI.UN(1,1-4)	4E 18.8	RESPECTIVELY, OF THE Ith STAR
	8	1-72	POSLUN(1,5-8)	4E18.8	POSIUN (1,1) AND POSLUN (2,1) ARE LATITUDE
	9	1-72	POSLUN(1,9-10), POSLUN(2,1-2)	4E18.8	AND LONGITUDE RESPECTIVELY, OF THE 1th LANDMARK IN
	10	1-72	POSLUN(2,3-6)	4E18.8	THE LUNAR, COORDINATE
	11	1-72	POSLUN(2,7-10)	4E18.8	SYSTEM.
8	1	2-5	IUNIT	15	INDICATOR FOR OUTPUT UNITS (SEE KLM)
		6-10	KOPT	15	INDICATOR OF DESIRED OPTION OF KSECPR ARRAY FOR PRINTING STATISTICS

# 2.3 . Cont'd

Sect.	Card	Cols.	<u>Name</u>	Type	Description			
•		11-60	IPSEC(I), I=1,10	1015	INDICATORS FOR SUPPRESSION OF EACH OF 10 PRINT SECTIONS			
	2	1-18	DTPI	E18.8	PRINT PORTION (HRS) OF: SUPPRESS			
		19-36	DTSUP	E18.8	PORTION (HRS) OF: TOTAL PRINT PERIOD			
		37-54	PRATE	E18.8	INDICATOR FOR USE OF ABOVE PRINT PERIOD			
	3	1-24	DTP	D24.12	PRINT INCREMENT			
9	1	2-5	NCOMB	15	NUMBER OF COMBINED BIASES			
		6-10	NSB	15	NUMBER OF STATION- ORIENTED BIASES			
		11-15	NDB	15	NUMBER OF DYNAMIC BIASES			
	2	2-	MCOL(I), I=1, NDSVB (NDSVB)* 15		CODES FOR BIASES WHERE NDSVB IS SUM OF NCOMB, NSB AND NDB			
10	. 1	2-5	MAXSTA	15	NUMBER OF STATIONS USED			
	2	2-5	KSTA	15	STATION NUMBER			
		6-25	KM(I), I=1,4	415	FREQUENCY OF ACCEPTANCE OF DATA TYPES			
	3	1-72	EBRMLT(J, KSTA), J=1,4	4E18.8	ARRAY OF EBAR MATRIX MULTIPLIERS			
	REPEAT CARDS 2-3 FOR EACH STATION							
11	ì	1-5	NOFT	15	NUMBER OF TIMES THROUGH BAYES FOR CONVERGENCE			
		6-10	MXPASS	15	MAXIMUM VALUE OF PASS COUNTER			
	2	1-24	TOLSQ	D24.16	SQUARE OF TOLERANCE FOR CONVERGENCE			
		25-48	TPRELM	D24.16	MAX. TIME OF PRELIMINARY BATCH			

#### 2.3 Cont'd

20

END OF FIRST GROUP OF INPUTS

Sect.	Card	Cols.	Name	Type	Description
	3	1-72	TSPAN(1-3)	3D24.16	TIME SPAN OF EACH BATCH
	4	1-72	TSPAN(4-6)	3D24.16	•
12	1	2-5	IPMAT	15	INDICATOR FOR MATRIX INPUT = 0 P MATRIX TO BE READ IN = 1 Q MATRIX TO BE READ IN
	2 .	1-72	(STAT(I,J),J= I=1, NBST		P OR Q MATRIX DEP. ON IPMAT WHERE NBST=TOTAL BIAS TYPES +6
13	1	1 -	OFFSET(I), I=1, NDB	4E18.8	OFFSETS OF DYNAMIC BIASES
		REPEAT	CARD 1 FOR EACH	VALUE OVER 4	N NEEDED
14	1	1 -	DEI P(1-3)	3E18.8	OFFSETS OF 1ST 3 REFRACTION PARAMETERS
			DELP(4-6)	3E 18.8	OFFSETS OF LAST 3 REFRACTION PARAMETERS SEE CARDS 10,11 OF SECTION 5
15	-(	PEN-			
16	-(	PEN-			
17	-(	OPEN-			
18	-(	OPEN-			
19	-(	OPEN-			

PROGRAM ADVANCES TO 2ND GROUP OF INPUTS. IF KSTDRD IS NEGATIVE, STANDARD VALUES ARE COMPUTED AND PROGRAM BEGINS TO READ IN 2ND SET OF INPUTS TO CHANGE OR AUGMENT ANY OF THESE STANDARDS. IF KSTDRD NOT NEGATIVE, ALL VALUES ARE READ IN, ELSE VALUES FROM PREVIOUS STACKED CASE ARE USED.

2	3	(	•	n	n	t	•	d

Sect.	Card	Cols.	Name	Type	<u>Description</u>
1 .	1-7	1-72	(DT3(I,J), I=1,3),J=1,7	3D24.12	INTEGRATION INTERVALS FOR EACH OF 7 WORKING BODIES FOR NEAR, MEDIUM AND FAR REFERENCE
2	1	1-72	R1(1-3)	3D24.12	R1 AND R2 ARE DISTANCES IN E.R FOR
	2	1-72	R1(4-6)	3024.12	EACH OF 7 WORKING BODIES FOR
	3	1-72	R1(7),R2(1-2)	3D24.12	SWITCHING FROM NEAR TO MEDIUM AND
	4	1-72	R2(3-5)	3D24.12	MEDIUM TO
	5	1-48	R2(6-7)	2D24.12)	INTEGRATION INTERVALS
3	1	1-24	RT1	D24.12	(VALUES USED AS TOLERANCES IN
		25.48	RT2	ر D24.12	RECTIFICATION CRITERIA
4	1	1-18	DH1	E18.8	TROPOSPHERE INTEGRATION STEP SIZE (KM)
	·	19-36	DH2	E18.8	IONOSPHERE INTEGRATION STEP SIZE (KM)
		37-54	H2	E18.8	UPPER LIMIT TROPOSPHERE (KM)
		55-72	н4	E18.8	UPPER LIMIT IONOSPHERE (KM)
5	1	2-5	KOBLAT	15	NUMBER OF OBLATENESS COEFFS
	2	2-5	M	15	M INDEX
		6-10	N	15	N INDEX
		11-15	ISORC	15	INDICATOR FOR C OR S COEFF. =0 S =1 C
	3	1-24	SORCCF	D24.12	VALUE OF COEFFICIENT
		REPEAT	CARDS 2-3 UNTIL	KOBLAT VALUE	S HAVE BEEN READ IN.
6	1	2-5 6-	MB MAX	15	NUMBER OF WORKING BODIES
		U-	KWBMU(T),I=1, MBMAX \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	BMAX)*15	INDICES OF WORKING BODIES

•	•	~ .			
2.	J	U	3 (	ıτ	. ' d

Sect.	Card	Cols.	Name	Type	Description
	2	1-72	TPMAT8(I), I=1,MBMAX	3D24.12	GRAVITATIONAL CONSTANTS OF WORKING BODIES
		REPEAT	CARD 2 FOR EACH VA	ALUE OVER 3	N NEEDED
7	1	1-24	DYN (48)	D24.12	SOLAR FLUX
		25-48	DYN (49)	D24.12	OPEN
8	1	1-72	DYN(51-53)	3D24.12	COEFFS. FOR LUNAR OBLATENESS
9	1	1-24	COMB(1)	D24.12	VELOCITY OF LIGHT
10	1	1-72	PRNT3(1-3)		PRINT INTERVALS (HRS) FOR NEAR MEDIUM AND FAR REFERENCE
11	1	1-24	EMIN	D24.12	MINIMUM ELEVATION ANGLE (RAD)
12	1	1-18	RTO	E18.8	RATIO OF NORDSIECK INTEGRATION INTERVAL TO THAT IN RUNGE-KUTTA
13		-OPEN-	-		
14	1	1-72	RATEV(1-3,1)	3D24.12	ROTATION VECTOR USED IN MARS DRAG COMPUTATIONS
	2	1-72	RATEV(1-3,2)	3D24.12	ROTATION VECTOR USED IN VENUS DRAG COMPUTATIONS
15	1-10	1-72	XMACH(I), I=1,4	0 4E18.8	MACH NUMBER TABLE
	11-20	1-72	CDT(I), I=1,40	4E18.8	DRAG COEFFICIENT TABLE
16	1	1 -	DELX(I), I=1,NB	ST 3D24.16	ARRAY OF CORRECTIONS TO THE STATE VARIABLES

REPEAT CARD 1 FOR EACH VALUE OVER 3N NEEDED

# . 2.3 Cont'd

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Sect.	Card C	ols.	Name	Type	<u>Description</u>
. 17	1	1-18	REJCT1	E18.8	NUMBER OF STANDARD DEVIATIONS
	1	9-36	REJCT2	E18.8)	ABOVE WHICH DATA ARE REJECTED ON FIRST AND SUBSEQUENT PASSES, RESPECTIVELY
18	-0	PEN-			
19	-0	PEN-			:

END OF 2ND GROUP OF INPUTS

#### 2.3.1 SPECIFICATION OF BIAS ERRORS

The user specifies which biases he wants included in section nine of the first group of inputs. In what follows, the intention is to clarify how to set up the proper codes for bias specification.

The first card in section nine reads in the following quantities:

NCOMB \_\*the number of combination type biases in the current run;

NSB - the number of station oriented biases

NDB - the number of dynamic biases

The sum of these three quantities is computed and a number of bias specifying codes equal to this sum is read in. Code numbers for combination type biases range from one to five, those for station—oriented biases from six to four hundred forty—seven and those for dynamic biases from four hundred forty—eight to five hundred—seven.

The breakdown is as follows:

## Combination type Biases

Code	Bias
1	Velocity of light
2	0pen
3	0pen
4	0 <del>pe</del> n
5	0pe n

<sup>\*</sup> A "combination" bias is one which is equally applicable to all ground stations. Velocity of light, earth radius and earth's ellipticity are examples of this type of bias.

# Station Oriented Biases

KSTA is station number NCDST = 17\*(KSTA\_1)
Let N = NCDST + 5

There are seventeen bias types associated with any station. For a given station, with number KSTA, the codes are:

Code	Bias
N+1	Station location error, u direction
N+2	Station location error, u direction
N+3	Station location error, w direction
N+4	Station rotation angle, east
N+5	Station rotation angle, north
N+6	Station rotation angle, vertical
N+7	Refractivity at station
N+8	Tropospheric model scale factor
N+9	Maximum electron density
N+10	Height of bottom of ionosphere
N+11	Height of maximum electron density
N+12	0pen
N+13	Delta_t for timing
N+14	Error in first observation type
N+15	Error in second observation type
N+16	Error in third observation type
N+17	Error in fourth observation type

## Dynamic Biases

<u>Code</u>	Biases
448	C oblateness coefficient, m=2, n=2
449	C oblateness coefficient, m=1, n=2
450	C oblateness coefficient,m=0,n=2
451	C oblateness coefficient, m=3, n=3
452	C oblateness coefficient, m=2, n=3
453	C oblateness coefficient, m=1, n=3
454	C oblateness coefficient, m=0, n=3
455	C oblateness coefficient, m=4, n=4
456	C oblateness coefficient, m=3, n=4
457	C oblateness coefficient, m=2, n=4
458	C oblateness coefficient, m=1, n=4
459	C oblateness coefficient, m=0, n=4
460	C oblateness coefficient, m=3, n=5
461	C oblateness coefficient, m=2, n=5
462	C oblateness coefficient, m=1, n=5
463	C oblateness coefficient, m=0, n=5
464	C oblateness coefficient, m=2, n=6
465	C oblateness coefficient, m=1, n=6
466	C oblateness coefficient, m=0, n=6
467	C oblateness coefficient, m=1, n=7
468	C oblateness coefficient, m=0, n=7
469	C oblateness coefficient, n=0, n=8
۵70	C oblateness coefficient, m=0, n=9

<u>Code</u>	<u>Pias</u>
471	C oblateness coefficient, m=0, n=10
472	S oblateness coefficient, m=2, n=2
473	S oblateness coefficient, m=1, n=2
474	S oblateness coefficient, m=3, n=3
475	S oblateness coefficient, m=2, n=3
476	S oblateness coefficient, m=1, n=3
477	S oblateness coefficient, m=4, n=4
478	S oblateness coefficient, m=3, n=4
479	S oblateness coefficient, m=2, n=4
480	S oblateness coefficient, m=1, n=4
481	S oblateness coefficient, m=3, n=5
482	S oblateness coefficient, m=2, n=5
483	S oblateness coefficient, m=1, n=5
484	S oblateness coefficient, m=2, n=6
485	S oblateness coefficient, m=1, n=6
486	S oblateness coefficient, m=1, n=7
487	Gravitational constant of Earth
488	Gravitational constant of Sun
489	Gravitational constant of Moon Gravitational constant of Mars
490	
491	Gravitational constant of Venus Gravitational constant of Jupiter
492	Gravitational constant of Saturn
493	Area—to—mass ratio for radiation pressure
494	Solar flux
495 496	Open
497	Area-to-mass ratio for air drag
498	A coefficient for lunar oblateness
499	B coefficient for lunar oblateness
500	C coefficient for lunar oblateness
501	Open
502	0pe n
503	0pen
504	0pen
505	0pen
506	0pe n
507	0pen

### 3. General Description of Output

In each of the three program subdivisions, the output is broken down into several sections. The user has the option of choosing any or all of these sections for printing during a particular run.

A great deal of flexibility exists in the choice of times at which to print. The user can specify an overall interval (labelled TAU) which is composed of a print portion (DTPI) and a suppress portion (DTSUP).

If the input variable PRATE is negative, printing takes place each time the print subroutine is entered during the print portion of the interval TAU. When PRATE is positive, it is used as a time interval, in hours, at which printing takes place in the DTPI portion of TAU.

The following sections describe the quantities which the user may specify as output in each of the three program subdivisions.

# 3.1 Output Options in Subdivision A

In Subdivision A, there are ten print sections. The following lists the output quantities which a particular section prints.

#### <u>Section 1</u>

Program time in hours since launch;

Current program date in hours, minutes, seconds, day and year;

Planetary body which is the current reference.

#### Section 2

Station number;

Observation types which station handles.

#### Section 3

Components and magnitudes of position and velocity vectors in units specified by the user.

# Section 4

Components and magnitudes of perturbations in position, velocity and acceleration in units specified by the user.

#### Section 5

Components and magnitudes of vectors between vehicle and each planetary body in specified units.

### Section 6

Components and magnitudes of vectors between the earth and each of the other planetary bodies in specified units.

## Section 7

Components and magnitudes of vectors between the sun and each of the other planetary bodies in specified units.

#### Section 8

Right ascension;

Declination;

Greenwich hour angle;

Longitude and latitude of earth subsatellite point;

Geocentric altitude, azimuth and elevation;

Geodetic azimuth and elevation.

## Section 9

True, eccentric and mean anomalies;

Eccentricity;

Inclination;

Argument of perigee;

Perigee passage time;

Right ascension of ascending node;

Period;

Mean motion;

Semi-major axis;

Perigee and apogee heights.

Section 10

Station name;

Program time in hours;

Station location;

Observation values.

Section 8 of the first group of inputs reads in the quantities by which the user designates the type and frequency of output desired. The inclusion of any of the ten output sections described above is specified by a positive value in the corresponding element of the array IPSEC.

# 3.2 Output Options in Subdivision Bl

In Subdivision B1, the printing is done by three subroutines, viz., PB1A, PRNTB1 and PTB1. This multiplicity of output routines was dictated by the need to conserve storage and fits well into the established overlay structure.

3.2.1 Output Associated with Trajectory Computations

Subroutine PBlA performs the function of testing if it is time to print. If so, it prints those Sections of Sections 1

and 3 (described in 3.1) which are specified in the IPSEC array.

Then, if the quantity in the calling sequence is non-zero and any of Sections 4 through 9 (also described in 3.1) are specified in the IPSEC array, PBIA calls subroutine PTB1. The latter prints the designated Sections.

## 3.2.2 Output Associated with Statistical Computations

Subroutine PRNTBl is assigned to the statistical link of the overlay structure. Its function is the printing of quantities associated with the Least Squares or Minimum Variance computations.

The output is divided into fifteen sections, only one of which can be printed at each call to PRNTB1. The section to be printed is specified in the calling sequence.

If KPRINT (an indicator set in PBlA at print times) is nonzero or if the indicator MFLAG is positive, the designated
element of the indicator matrix, KSECPR, is tested. When it
is non-zero, the section specified in the calling sequence is
printed. The sections available for printing are as follows:

Section	Output
1	State Transition Matrix, PHI
2	Point Transformation Matrix, S
3	Covariance Matrix, Q Update
4	Observation Matrix, M
5	Observation Matrix, N
6	EBAR Matrix
7	Covariance of Observations Matrix, Y

Section	Output
8	Inverse of Y Matrix
9	Optimum Filter Matrix, L
10	Covariance Matrix, Q Corrected
11	Covariance Matrix, P
. 12	Array of Parameter Residuals
13	Array of Residuals of States
14	Station Number and Data Types
15	Station Name, Observation Values and Time

The indicator KOPT is read in Section 8 of the first group of inputs.

## 3.3 Output Options in Subdivision B2

In Subdivision B2, the printing is done by three subroutines, viz., BPRA2, BPRB and BPTA2. Here, as in B1, use of the overlay structure to conserve storage led to a multiplicity of output subroutines.

3.3.1 Output Associated with Trajectory Computations

The discussion in Section 3.2.1 applies exactly here when BPRA2 is substituted for PBIA and BPTA2 for PTB1.

3.3.2 Output Associated with Statistical Computations

The discussion in Section 3.2.2 applies exactly here when BPRB is substituted for PRNTB1.

# 4. Operating Procedures

All runs are set up as jobs under the IBSYS/IBJOB Operating System. Each of the program subdivisions is composed of a distinct set of decks. The overlay feature of IBJOB is used by each subdivision and the appropriate control cards are required for defining the overlay structure.

The operational aspects of the Orbit Determination Program will be described in detail for use under the "Stand-Alone" 7090/7094. The approach for its operation under the 7040-7094 Direct-Coupled System will also be described.

# 4.1 Typical Deck Set Up

Consider the overlay diagram for Subdivision A (Figure 1).

The deck set-up to run a job would be as follows:

Columns:	1	8	16
	\$JOB		
	\$EXECUTE		IBJOB
	\$IBJOB		GO, MAP, NOFLOW
	\$IBLDR	DMTML	
	binary deck for	r DMTML	
	\$ IBLDR	DOMUD	
	binary deck for	r DOMUD	
	\$ IBLDR	EXECA	
	binary deck for	r EXECA	
	\$OR IG IN		ALPHA
	\$ IBLDR	INPUTA	
	binary deck fo	r INPUTA	

Columns:	1			8	16
	\$ IBLDR			XFORM	
	binary	deck	for	XFORM	
	\$OR IG IN				ALPHA
	\$ IBLDR			ATIM	
	binary	deck	for	ATIM	
	\$.IBLDR			DDOT	
	binary	deck	for	DDOT	
	\$IBLDR			ЕРНЕМ	
	binary	deck	for	ЕРНЕМ	
	\$ IBLDR			FIX	
	binary	deck	for	FIX	
	\$ IBLDR			MAINA	
	binary	deck	for	MAINA	
·	\$ IBLDR			MODELA	
	binary	deck	for	MODELA	
	\$ IBLDR			NUTPRE	
	binary	deck	for	NUTPRE	
	\$ IBLDR			OBD	
	binary	deck	for	OBD	
•	\$ IBLDR			OBSERA	
	binary	deck	for	OBSERA	
	\$ IBLDR			PRINTA	
	binary	deck	for	PRINTA	
	\$ IBLDR			SERVCE	
	binary	deck	for	SERVCE	

Columns:	1			8	16
	\$ IBLDR			STACUL	
	binary	deck	for	STACUL	
	\$ IBLDR			STAPOS	
	binary	deck	for	STAPOS	
•	\$ IBLDR			T IMNGA	
	binary	deck	for	TIMNGA	
	\$OR IG IN				BETA
	\$IBLDR			CDERIV	
	binary	deck	for	CDERIV	
	\$ IBLDR			CINT	
	binary	deck	for	CINT	
	\$IBLDR			CINTRP	
,	binary	deck	for	CINTRP	
	\$IBLDR			CITGRA	
	binary	deck	for	CITGRA	
	\$IBLDR			CRSTRE	
	binary	deck	for	CRSTRE	
	\$ORIGIN				GAMMA
	\$IBLDR			COBDRG	
	binary	deck	for	COBDRG	
	SOR IG IN				GAMMA
	\$IBLDR			CMVDRG	
	binary	deck	for	CMVDRG	
	SOR IG IN				GAMMA
	\$IBLDR			CCHREF	
	binary	deck	for	CCHREF	

•	Columns:	1			8		16
•		\$ IBLDR			CMNOBP		
•		binary	deck	for	CMNOBP		
		SORIGIN			•	1	BETA
		\$IBLDR			FDERIV		•
		binary	deck	for	EDER IV		
		\$.IBLDR			EINT		:
		binary	deck	for	EINT		
		\$ IBLDR			EINTRP		
		binary	deck	for	EINTRP		. t
		\$IBLDR			EITGRA		
		binary	deck	for	EITGRA		
		\$BLDR			ERSTRE		
		binary	deck	for	ERSTRE		
		\$ IBLDR			KEPLFR		
		binary	deck	for	KEPLER		
		\$ IBLDR			PFLGHT		
-		binary	deck	for	PFLGHT		
		\$ IBLDR			RECT		
		binary	deck	for	RECT		
		SOR IG IN				1	DELTA
		\$ IBLDR			EOBDRG		
		binary	deck	for	EOBDRG		
		SOR IG IN					DELTA
		\$ IBLDR			EMVDRG		
		binary	deck	for	EMVDRG		

Columns:	1	8	16
	\$OR IG IN		DELTA
	\$IBLDR	ECHREF	
	binary deck for	ECHREF	
	\$ IBLDR	EMNOBP	
	binary deck for	EMNOBP	
	\$ORIGIN		BETA
	\$IBLDR	PFINIT	
	binary deck for	PFINIT	
	\$ENTRY	•	EXECA
	\$DATA		
	Deck containing	Specifications	Input
•	\$IBSYS		

In the above deck set-up the \$IBLDR control card and the binary deck for a subroutine may be replaced by a \$IBFTC control card and the source deck for the subroutine.

# 4.2 Tape Assignments

The tape unit containing the pre-stored program and data deck is mounted on SYSIN1.

Other tape units referred to by the various subdivisions are logical units 8, 9, 10 and 11. The corresponding tapes should be mounted on drives in accordance with the Tape Assignment Table in effect at the particular installation.

Logical Tape 8 contains the required tables of planetary positions. It is used by all program subdivisions.

Logical Tape 9 is the observation data tape. In Subdivision A, a scratch tape should be mounted on logical unit 9 when in the mode calling for a simulated data tape to be produced. In Subdivisions B1 and B2, those modes calling for observational data require a data (real or simulated) tape on logical unit 9.

Logical Tape 10 is used for Summary information. Therefore, a scratch tape should be mounted on logical unit 10 when running Subdivisions B1 or B2.

Logical Tape 11 is used as a temporary store for various quantities by Minimum Variance and Bayes statistics. A scratch tape on logical unit 11 is therefore required in Subdivisions B1 and B2.

An additional option of the overlay features is the use of tapes to share the function of the Load File Tape (see the IBJOB manual for description). These additional tapes shorten the amount of time necessary for the loader to locate a particular link to be brought into core.

This option is specified by placing the system unit name (such as SYSUT2), onto which the dependent link is to be written, on the \$ORIGIN control card preceding that link. Each distinct system unit name thus specified requires a scratch tape to be mounted on the drive corresponding to the system unit.

When running under the Direct-Coupled System, the following differences are to be noted:

- (a) SYSIN1 and SYSOU1 no longer require tape drives:
- (b) Any other unit not specified on a \$SETUP control card will automatically be assigned to the Disc.

  Hence, \$SETUP cards are required for the Ephemeris tape (logical unit 8) and the observation data tape (logical unit 9). It is recommended that \$SETUP cards also be used for the tapes on which the dependent links are written, for speed of operation.

# 4.3 Subdivision B2

Up until now, Subdivision B2 has been treated as a complete program in itself, having much the same structure as Subdivision B1. However, the current version of the IBSYS system requires so much memory that it is not possible to fit the longest link of Subdivision B2 into core.

As a result, Subdivision B2 has been divided into two separate sub-programs, B2(A) and B2(B). B2(A) uses only Minimum Variance for its statistical processing and B2(B) uses only Bayes Estimation.

It is expected that later versions (viz., 12 and 13) of IBSYS will require much less memory for system purposes, thus allowing B2(A) and B2(B) to be recombined to Subdivision B2.

Figures 3 and 4 present the overlay diagrams of Subprograms B2(A) and B2(B). Figure 2 shows the overlay structure of Subdivision B1. Logical Tape 9 is the observation data tape. In Subdivision A, a scratch tape should be mounted on logical unit 9 when in the mode calling for a simulated data tape to be produced. In Subdivisions B1 and B2, those modes calling for observational data require a data (real or simulated) tape on logical unit 9.

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# 4.4 Recommended Optional Procedures

Certain techniques can be employed to give more efficiency of operation in the running of the Orbit Determination Program.

Consider the user who desires to run Subdivision Bl with the Encke option of integration exclusively.

The following modifications can then be made to the program deck:

- (a) CITGRA can be replaced by a dummy subroutine. (It cannot be removed entirely, since a CALL CITGRA statement is present in subroutine MAINB1.)
- (b) The binary decks for subroutines CINT, CCHREF, CRSTRE, CDERIV, COBDRG, CINTRP, CMVDRG, CMNOBP can be removed.

This will shorten the size of the program deck and hence minimize loading time on the computer. The same approach can also be taken if the user wants to use one method of statistical processing, for example, Bayes Estimation.

To avoid the deck handling problems, all programs can be pre-stored on tape, each subdivision occupying a different file. Then, a particular run can be made with a very small input deck by making use of the \$IEDIT control card of the IBJOB Input/Output Editor.

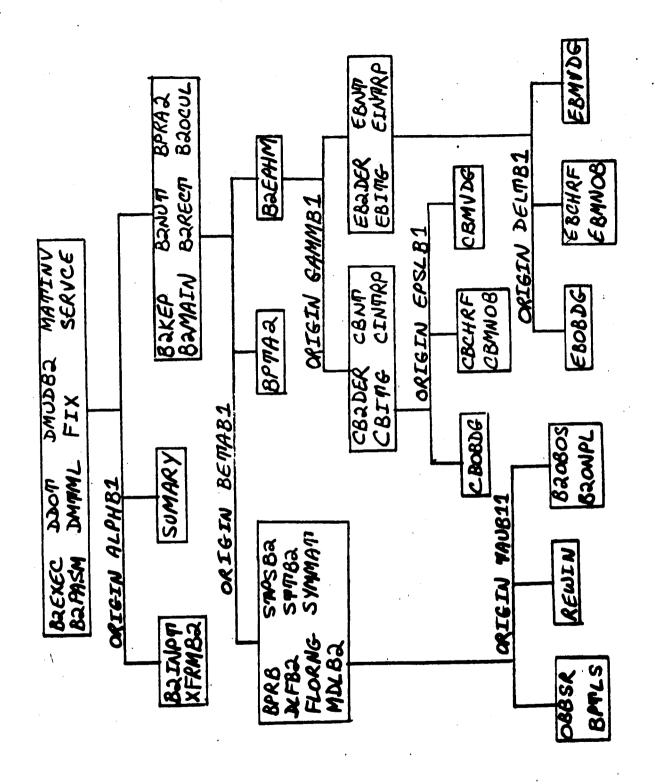


Figure 3
Overlay Structure for Subdivision B2(A)

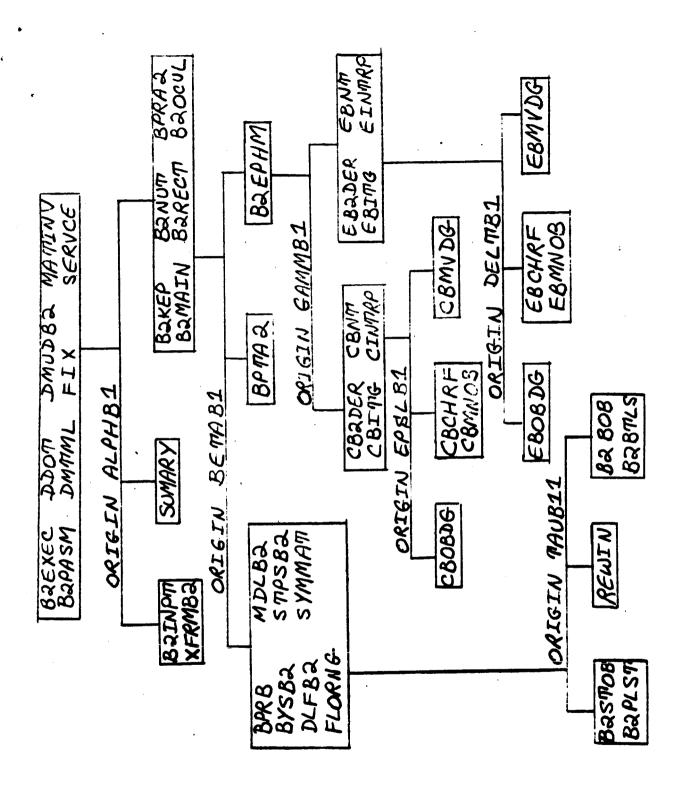


Figure 4
Overlay Structure for Subdivision B2(B)